

HOW TO COORDINATE TRANSFORMER PRIMARY-SIDE FUSES WITH FEEDER RECLOSERS

PART I: CONSERVATIVE METHOD

In part I, we explain how to coordinate transformer primary-side fuses with a secondary-side automatic circuit recloser, such as in a utility substation.

We'll use the "conservative" coordination method, which ignores the effects of fuse cooling during the reclosing time intervals (contacts open) of the recloser.

SOURCE-SIDE FUSE/LOAD-SIDE RECLOSER COORDINATION

Automatic circuit reclosers sense overcurrents, interrupt them, and then automatically reclose to reenergize the feeder. Most faults on overhead distribution systems — perhaps as many as 75 to 80% — are temporary in nature, lasting only a few cycles to a few seconds.

With their "trip and reclose" capability, reclosers eliminate prolonged outages on distribution systems due to such temporary faults. If a fault is permanent rather than temporary, however, the recloser will "lock out" after a preset number of reclosing attempts (usually three or four), thus isolating the faulted feeder from the system.

Automatic circuit reclosers have dual timing capabilities which help maintain coordination with other protective devices and limit the areas affected by permanent faults. Typically the first — sometimes the first two — fault-clearing operations are performed per the "fast" timing characteristic, clearing temporary faults before load-side protective devices operate. Subsequent operations incorporate a predetermined time delay that allows protective devices nearer the fault to interrupt permanent faults, thereby limiting the extent of the service interruption.

This arrangement is often referred to as a "fuse saving" scheme, since fuses only respond to permanent faults within their zones of protection.

For the application covered in this article, the transformer primary-side fuse is located upstream of the automatic cir-

cuit recloser. The goal is that the fuse not melt before the recloser operates to lockout in response to a permanent fault. The maximum fault current value up to which the fuse and the recloser will coordinate is generally the lower of:

1. The maximum interrupting capacity of the recloser or fuse, or
2. The intersection of the minimum-melting curve of the fuse and the maximum-equivalent operating curve of the recloser (i.e., the "lockout" curve).

In the conservative coordination method, cooling of the fuse during reclosing time intervals (contacts open) is ignored. You simply sum the heating effect, or heat input, of each recloser operation. That is, the lockout curve of the recloser is developed by summing the total clearing times for the proper number of fast and slow operations, at various current levels, per the following equation:

$$T_l = \frac{\sum_{j=1}^n T_{Rj}}{1 - P}$$

Where:

T_l = Point on the maximum equivalent lockout curve of the recloser, at selected current (I).

P = Reduction in the melting time of the fuse due to preloading, expressed as a decimal part of its total melting time.

TR_j = Maximum clearing time at current (I) for the j th operation (contacts closed) of the recloser.

n = Number of operations (contacts closed) of the recloser.

Since the fuse must allow the recloser to operate to lockout without melting, the recloser's maximum equivalent lockout curve should be developed. Recloser fast curves (A) are typically published to maximum test points. But slow curves (B, C, and D) are published to nominal test points and must be adjusted (maximized) by the amount of the positive tol-

erance, which is assumed to be 10%.

EXAMPLE

Consider a rural electric power substation having a single transformer, protected by fuses, with three or fewer feeder reclosers. Ratings for the primary-side fuse, the transformer, and the load-side reclosers are as follows:

Transformer: The transformer has a base (OA) rating of 7500 kVA three-phase, 115 kV primary, 13.2 kV secondary. It has a forced-air (FA) rating of 9375 kVA (125%). The transformer impedance is 7.5%, and the maximum three-phase secondary fault current is 478 amperes (2000 MVA), as seen on the primary side of the transformer. The transformer is connected delta grounded-wye.

Fuse: The primary-side fuse is a 65E-ampere Standard Speed S&C SMD-2B Power Fuse rated 115 kV. The full-load current of the transformer, based on its force-air rating is 47 amperes. At this level of transformer loading, the fuse will be loaded to 72% of rating (47 amperes ÷ 65 amperes = 0.72). The preload adjustment factor, as determined from S&C Data Bulletin 210-195, is 0.88.

Feeder Recloser: The load-side recloser is a hydraulically controlled Cooper Type W Recloser, rated 14.4 kV, 560 amperes continuous. The phase-trip pickup current is 280 amperes (140-ampere coil), and the operating sequence is one fast (A) and three slow (C) operations. The reclosing time interval between the fast operation and the first delayed operation is 0.5 second (instantaneous). Between the delayed operations, the reclosing time interval is 5 seconds.

COMPLETING THE EXERCISE USING COORDINAIDE

To complete the coordination exercise, launch Coordinaide by clicking the appropriate link on the page of S&C's website you're visiting... A Coordinaide link is featured on the home page.

Continued on Page 56

Feeder Reclosers

Continued from Page 54

Additional links are found under the drop-down menu labeled “Support” and also on applicable product pages; e.g., S&C Type SMD Power Fuses. These tab-style links are on the left-hand side of the page, immediately below the “For More Information” label and above the “TCCs for [product]” tab.

After clicking on one of the links, you’ll be directed to Coordinaide’s opening page. It provides a brief description of the applications Coordinaide is designed to handle. When you launch the program, you’ll be directed to a second page containing a brief “Conditions of Use” disclaimer, followed by a short note detailing minimum web browser requirements and a link to a “Users Guide.”

One final click launches the program and takes you to the “General Information” page. Please follow these directions to select the primary-side fuse, the transformer, and the load-side recloser.

Step 1 — Enter General Information

- Project Name: Fuse-Recloser Coordination Exercise
- Date: [provided by Coordinaide]
- By: Optional

Step 2 — Enter System Information and Select Devices

- Three-Phase Voltage, kV: 115
- Available Fault Current, Amperes RMS Symmetrical: 10000
- Device #1 — Power Fuse
- Device #2 — Transformer (Damage Curve)
- Device #3 — Recloser

Click “Continue” after entering system information and selecting the devices. You’ll be directed to the first “device” page.

Step 3 — Select and Enter Device Parameters

Device #1 — Transformer-Primary Fuse (Select Parameters)

- Manufacturer: S&C
- Type: SMD-2B
- Speed: Standard
- Voltage Range, kV: 115-138
- Ampere Rating: 65E

Click “Continue” after selecting the parameters for Device #1. The time-current characteristic curve for Device #1 will be displayed.

Device #2 — Transformer (Select Parameters)

• Three-Phase Primary Voltage, kV: 115 [Provided by Coordinaide]

- Three-Phase Secondary Voltage, kV: 13.2
- Three-Phase Rating, kVA: 7500
- Impedance, %: 7.5
- Fault Current, Amperes RMS Symmetrical: 10000

[Provided by Coordinaide]

- Display Magnetizing Inrush Points? _ Yes _ No (default)
- Connection: Delta Grounded-Wye

Click “Continue” after selecting the parameters for Device #2. The time-current characteristic curve for Device #2 will be displayed.

Device #3 — Feeder Recloser (Select Parameters)

- Coordinates With: _ Source-Side Device _ Load-Side

Device See Note 1

• Coordination Method: _ Cooling Factor _ Conservative (default) See Note 2

• Manufacturer: Cooper (McGraw): Hydraulic

• Type: W

• kV Range, kV: 14.4 [Provided by Coordinaide]

• Phase-Trip Operating Sequence: 1 Fast / 3 Slow

• Fast Curve: “A”

• Slow Curve: “C”

• Coil Rating, Amperes: 140

• Ground-Trip Operating Sequence: Skip for this example

Note 1: Since the recloser is on the load side of the primary-side fuse, select “Coordinates with Source-Side Device (default in this example).”

Note 2: Select “Conservative Method” to disregard the effects of cooling of the primary-side fuse during reclosing time intervals (contacts open) of the recloser. You are encouraged to repeat this example using the more precise cooling-factor method, and then compare the results.

Click “Continue” after selecting the parameters for Device #3. The time-current characteristic curve for Device #3 will be displayed.

Step 4 — Go to “Results” Page

Click on the tab at the top labeled “Results.” You’ll be directed to a log-log grid with

TCC curves of the devices you’ve selected.

If desired, you can change the current scale of the grid from the default, 5 to 100,000 amperes, to 0.5 to 10,000 amperes. You can also eliminate the hash-fill applied to the TCC curves, to make the plot more readable. And you can zoom in on a particular section of the grid by entering the upper and lower current and time values in the appropriate cells.

To see a full-size TCC plot or full-size summary information, click on “Printer Friendly Graph” or “Printer Friendly Summary,” as applicable.

Now let’s review the TCC plot of the coordination example under consideration.

Device #1, the 65E-ampere Standard Speed primary-side power fuse, is plotted in red.

Device #2, the transformer damage curve, is plotted in black. And Device #3, the loadside recloser, is plotted in orange. The two thicker orange curves are the recloser fast curve (A) and slow curve (C), respectively, based on TCC data published by the recloser manufacturer. The thin orange curve is the maximum-equivalent lockout curve of the recloser, reflecting positive tolerances.

The 65E-ampere Standard Speed power fuse provided excellent protection for the transformer as evidenced by the fact the total-clearing curve of the fuse crosses the transformer damage curve at current levels less than the maximum values obtained for any type of fault. This fuse has a published peak-load capability of 107 amperes, which means that the transformer can be loaded to nearly 280% of nameplate — well in excess of the desired OA/FA rating (125% of nameplate).

Unfortunately, the primary-side fuse does not coordinate with the maximum-equivalent lockout curve of the recloser, since the minimum-melting time of the fuse at 478 amperes (0.42 second) is less than the maximum-equivalent lockout curve of the recloser at this current level (0.69 second). Note that the secondary-side recloser curves have been shifted to the

Continued on Page 58

Feeder Reclosers

Continued from Page 56

right, by 15% in terms of current, to account for the primary-side to secondary-side current imbalance that would exist were a phase-to-phase ungrounded secondary-side fault to occur.

When faced with this situation, the natural reaction is to select the next-larger-amperaged primary-side power fuse, a

fuse with a slower time-current characteristic, or perhaps both... until coordination is achieved. While this solution may result in complete coordination between the fuse and the recloser, it does so at the expense of transformer protection — not the optimal result. Before selecting a larger fuse, or one with a slower time-current characteristic, repeat this exercise using the more precise cooling-factor method.

You may find that the primary-side fuse initially selected provides complete coordination after all!

